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MTD BTL

Sensor Module Assembly and Tests

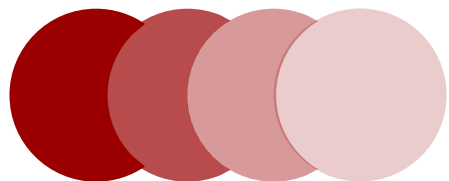
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Mingtao Zhang, Licheng Zhang, Jin Wang

Peking University

CLHCP2023, Nov 16



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01 MTD BTL

Physics motivation of MTD BTL



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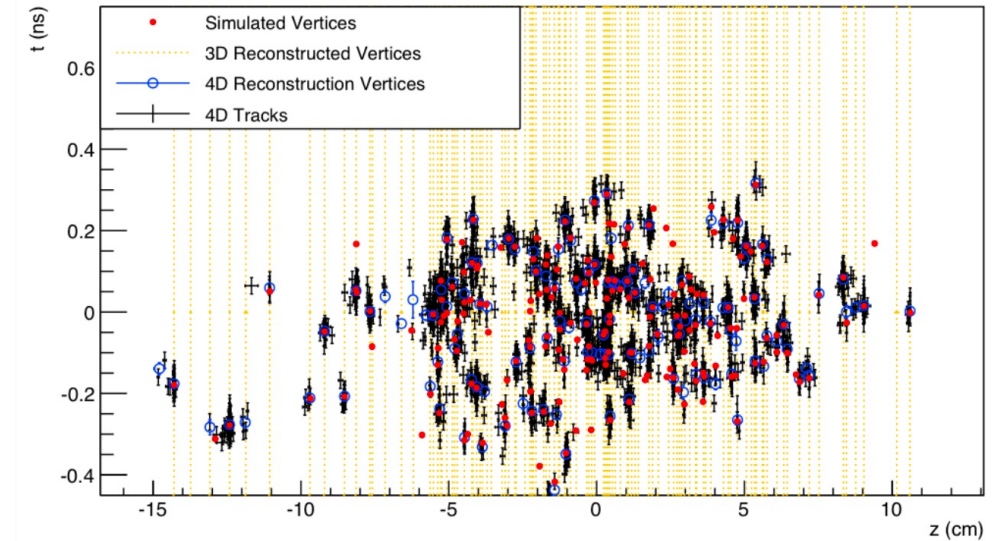
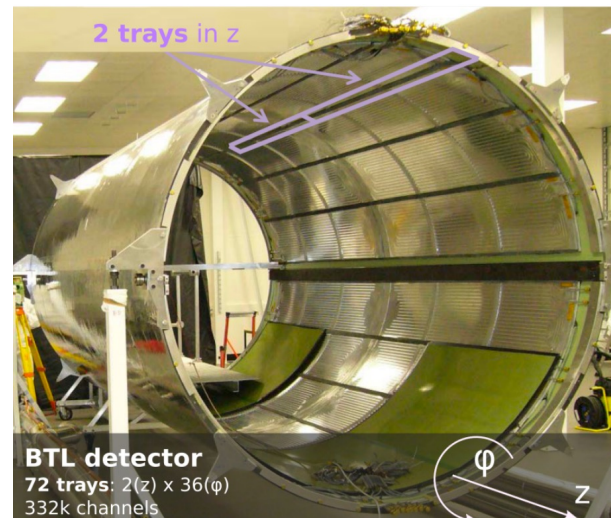
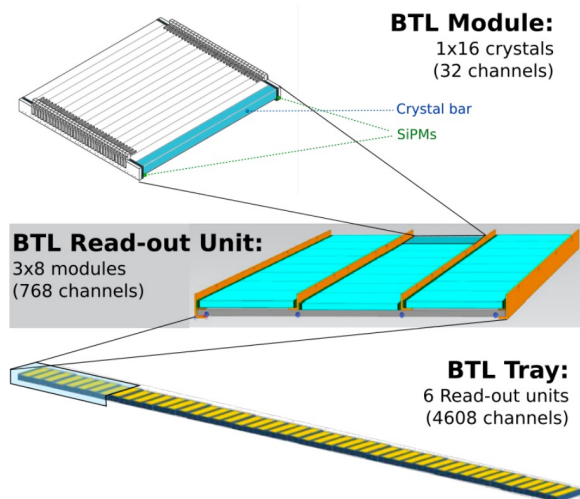
High luminosity \rightarrow high pileup

The MTD will be added to CMS to help meet the challenge of high luminosity.

- offset fully degradation from 140 to 200 pileup recover the effective background conditions close to Phase-1 operations.

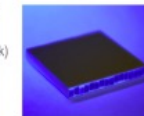
The BTL is a thin, cylindrical detector

- BTL Module, Read-out Unit, Tray, BTL detector



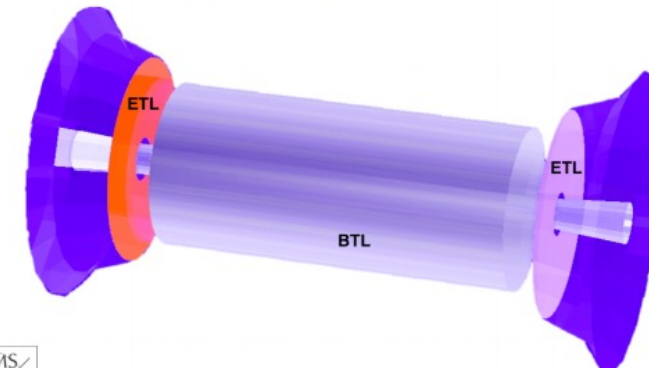
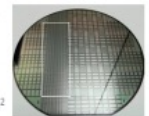
BTL: LYSO bars + SiPM readout:

- TK / ECAL interface: $|n| < 1.45$
- Inner radius: 1148 mm (40 mm thick)
- Length: ± 2.6 m along z
- Surface ~ 38 m²; 332k channels
- Fluence at 4 ab⁻¹: 2×10^{14} n_{eq}/cm²



ETL: Si with internal gain (LGAD):

- On the CE nose: $1.6 < |n| < 3.0$
- Radius: 315 < R < 1200 mm
- Position in z : ± 3.0 m (45 mm thick)
- Surface ~ 14 m²; ~ 8.5 M channels
- Fluence at 4 ab⁻¹: up to 2×10^{15} n_{eq}/cm²



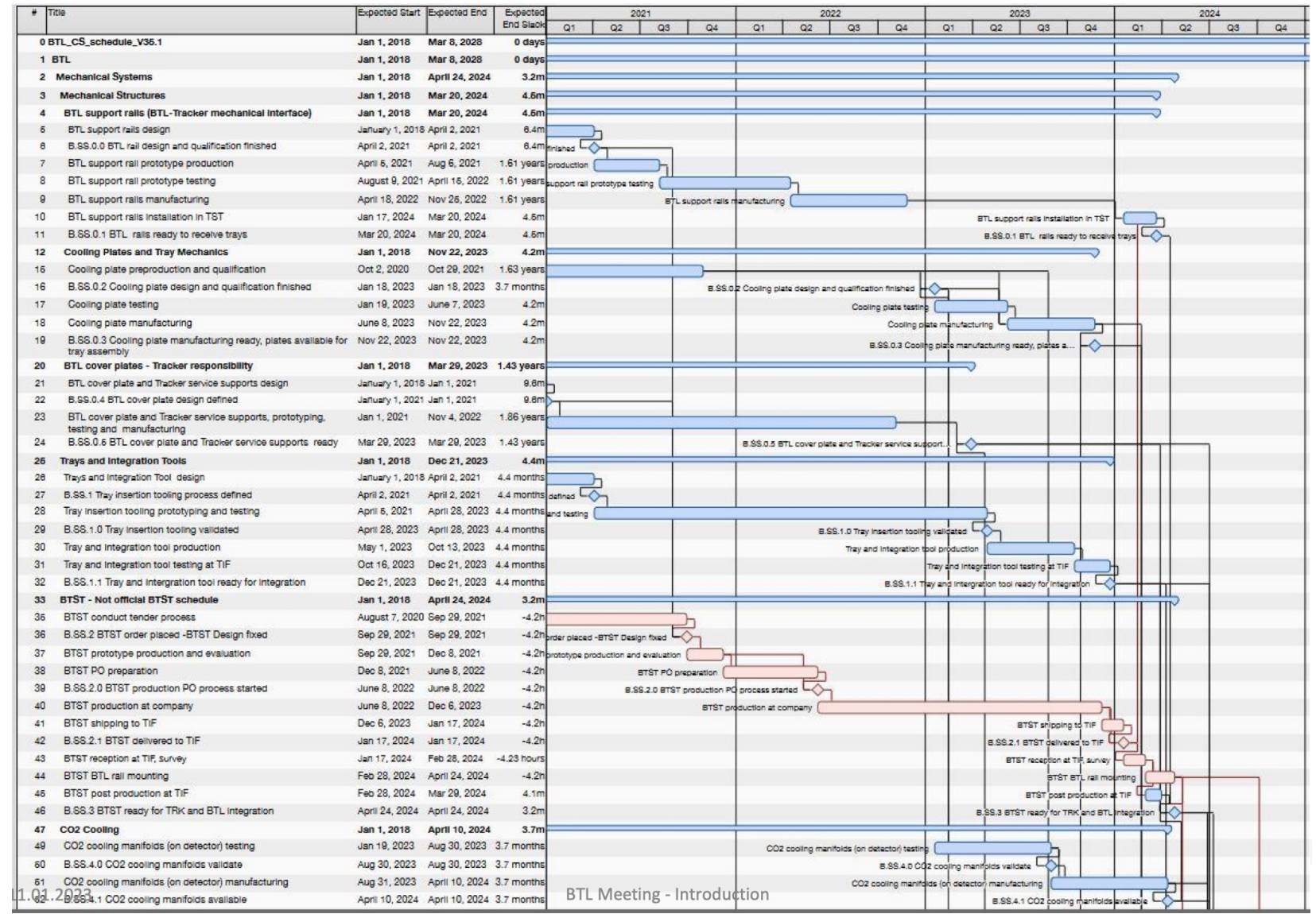
Schedule of MTD BTL



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PKU Assembly timeline

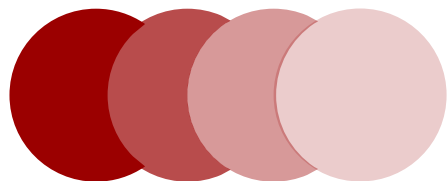
- Improve the assembly and QA/QC in the summer of 2023
- Assembly Center Certification in the autumn of 2023
- Start batch assembly in early 2024
- End assembly in the summer of 2026
- Installed in the autumn of 2026



BTL Meeting - Introduction



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02 Test Beam

SiPM cell-size: introduction and setup

章立诚
(PKU)



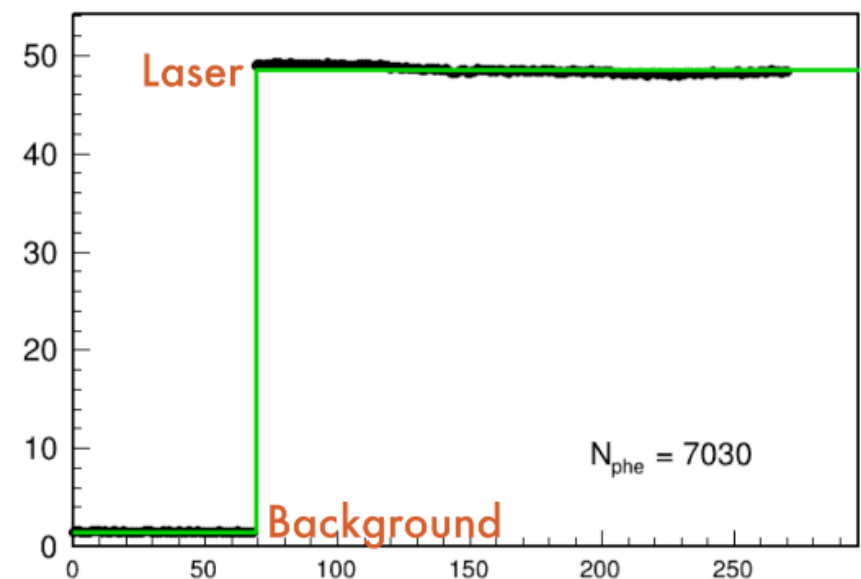
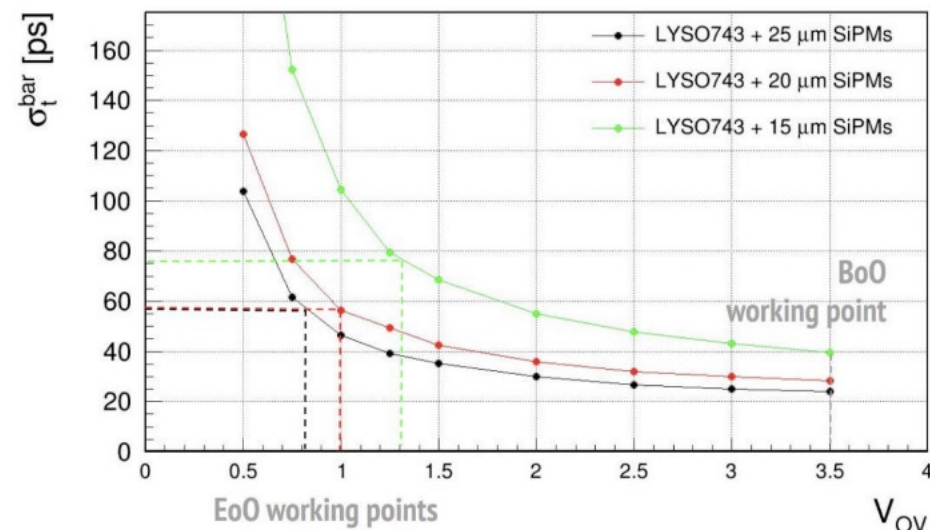
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Motivation

- The cell size of SiPM has a significant impact on the time resolution

Setup

- LYSO array (#743, LYSO MS from prod 3) grease-coupled to HPK SiPM arrays with different cell-sizes (15 , 20, 25 μm - all type 2)
- Time resolution measured with TOFHIR2X and UV-induced scintillation
 - vs overvoltage, threshold
 - vs N_{phe} (tuning the laser intensity)



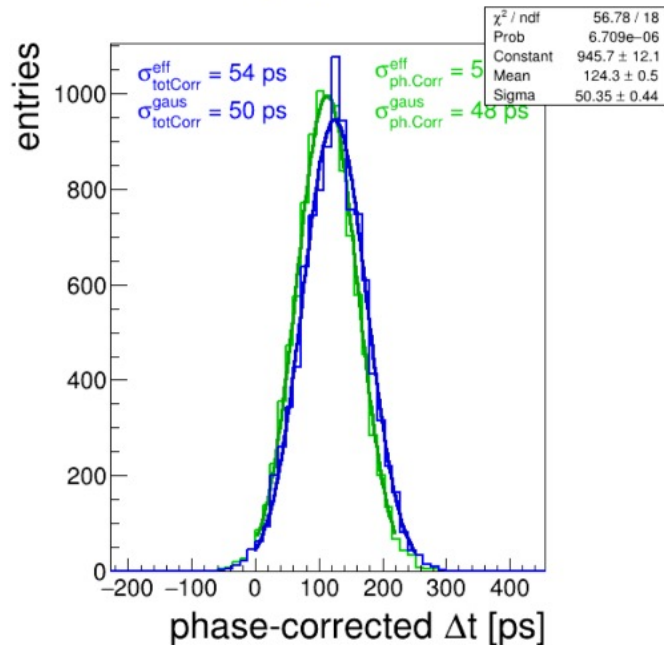
SiPM cell-size: optimization and correction



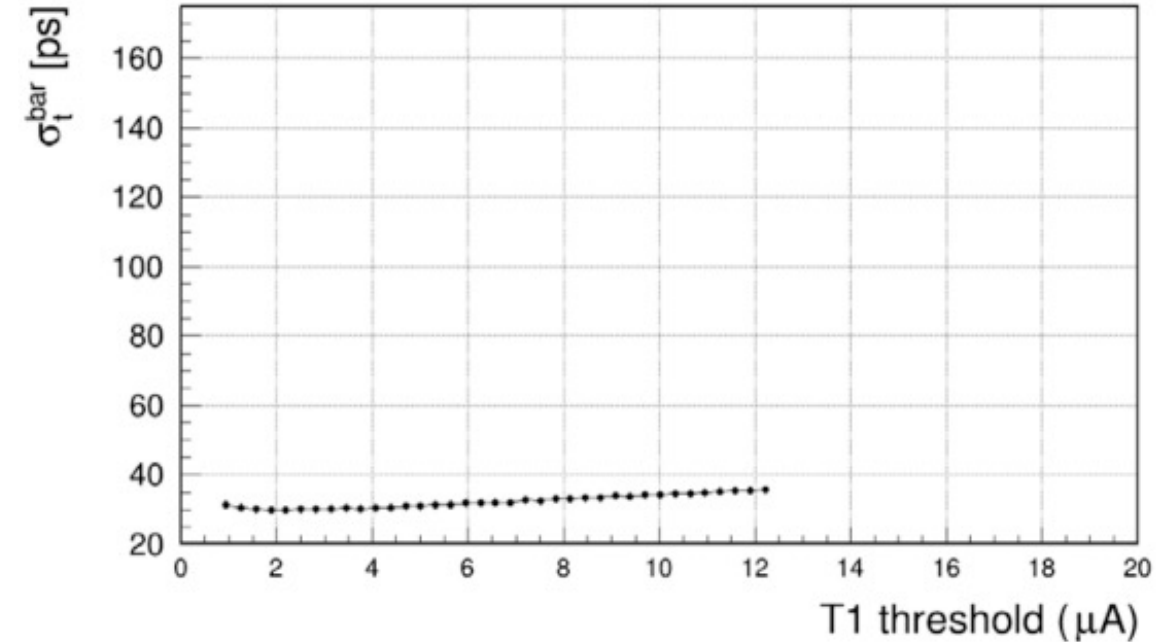
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Pulse Shapes

- Find the threshold that can **minimize** the time resolution



- Correction over energy difference
- Correction over ToT
- Should be highly correlated



- Correction of the starting point in the triggering window
- Secrets in electronics

SiPM cell-size: summary and understanding



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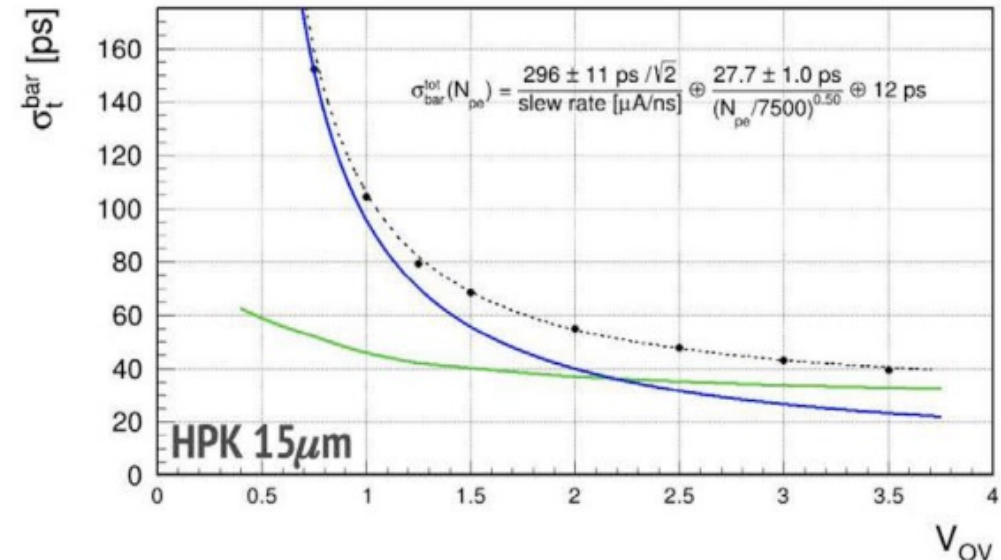
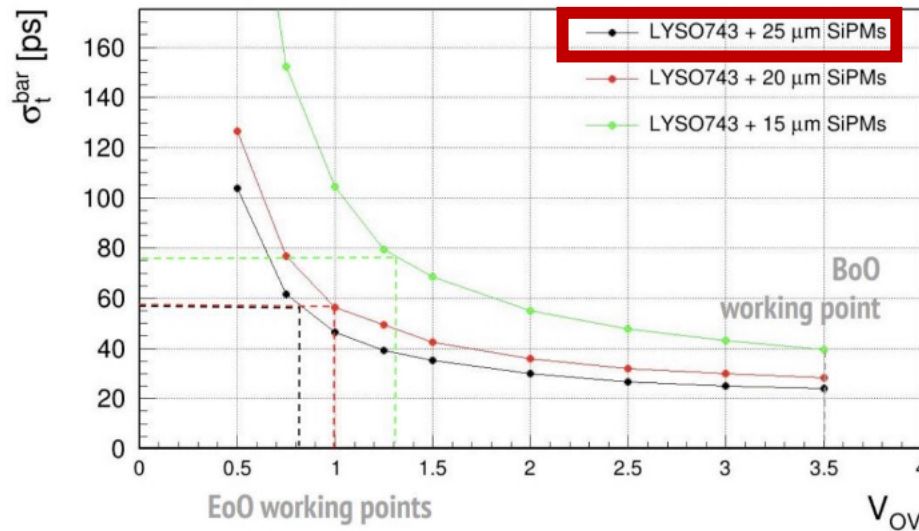
Summary

- First lab measurements of modules with new SiPMs with larger cells
- Improved performance for larger cells SiPMs (25 μm)

Understanding

$$\sigma_t^{\text{noise}} = \frac{\sigma_N}{dA/dt}$$

$$\sigma_t^{pe} = \frac{A}{\sqrt{N_{pe}}}$$



LYSO selection

张铭滔
(PKU)

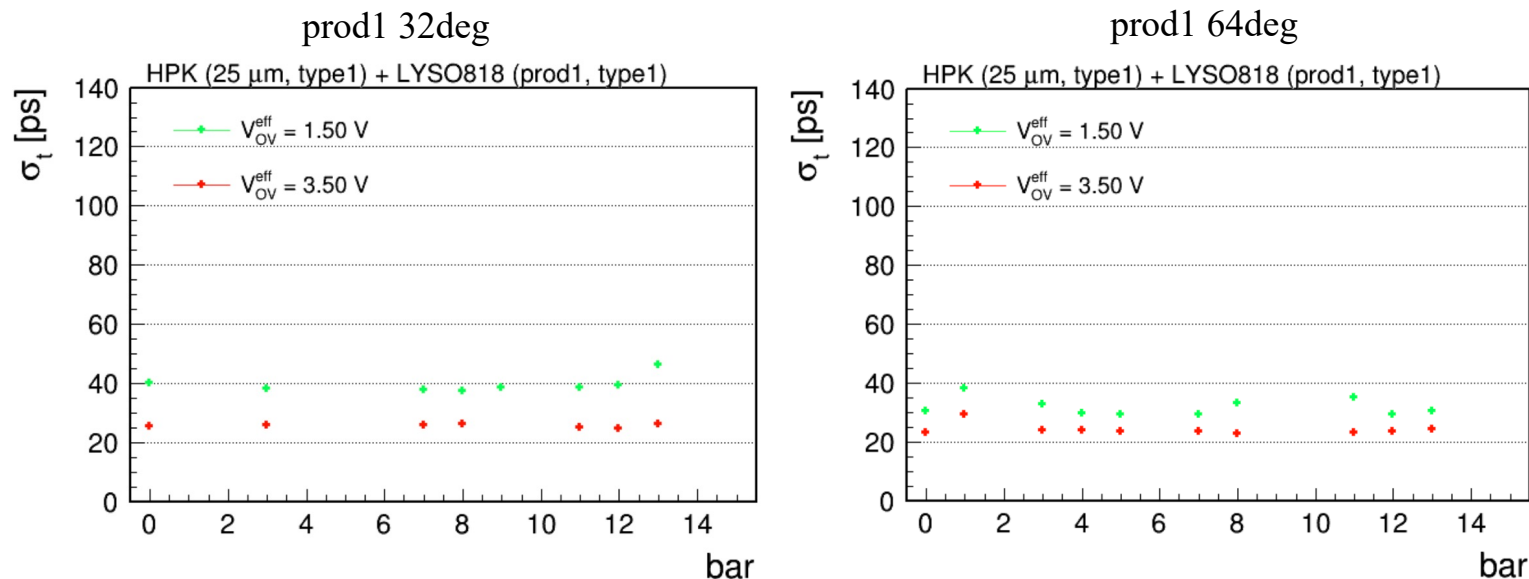


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Comparison between vendor 1 (LYSO818) and vendor 5 (LYSO828)

Measurement of time resolution (σ_{tdiff})

- Compare the time resolution (σ_{tdiff}) given by the two modules under different **angles** and **Vov**.



Results are measured at the optimal threshold

LYSO	Vov/V	angle/deg	t_{Res}/ps	error/%
prod1	1.50	32	38.2	6.9
		52	32.2	3.1
		64	30.9	9.0
	3.50	32	25.7	2.1
		52	23.5	1.2
		64	23.6	7.2
prod5	1.50	52	35.1	4.3
	3.50		24.6	4.0

- Due to the influence of noise, the resolution of 3.50V is generally better than 1.50V. Moreover, the signal increases when the angle to the beam increases, which is beneficial to distinguish the MIP peak from the noise peak, so the resolution is better;
- Time resolution of **prod1 is better than prod5**.

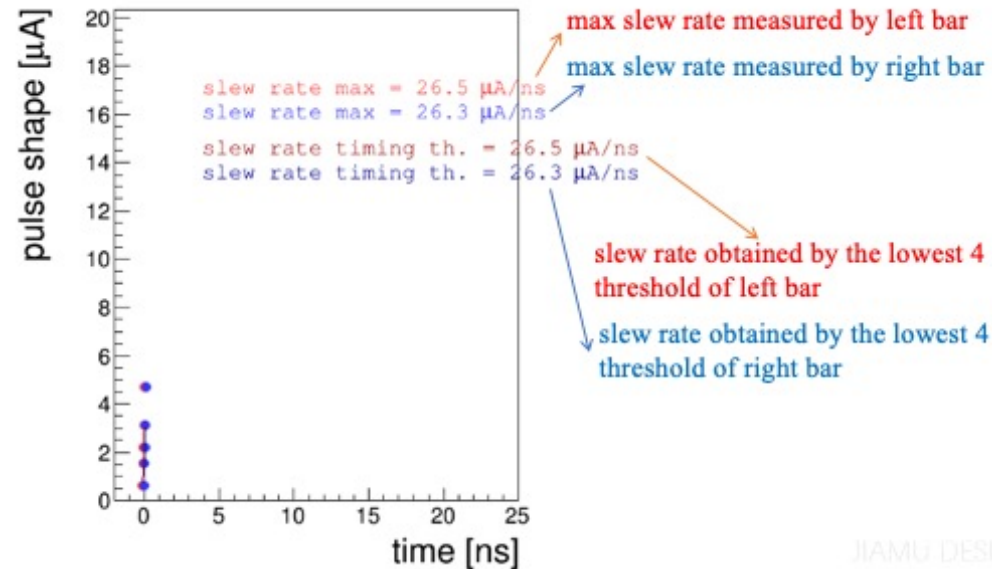
LYSO selection



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Slew rate

- Plot the relation between Amplitude and time, and Compare the maximum slope of each module.



LYSO	Vov/V	angle/deg	SR/($\mu\text{A/ps}$)
prod1	1.50	32	16.7
		52	18.7
		64	16.9
	3.50	32	33.6
		52	33.3
		64	57.9
prod5	3.50	52	44.6

- With the increase of Vov and angle to the beam, the signal amplitude increases, so SR is generally larger;
- The slew rate of **prod5** is better than prod1;
- In the data of prod5, there are only 4 points when Vov=1.50V, so it cannot be compared together.

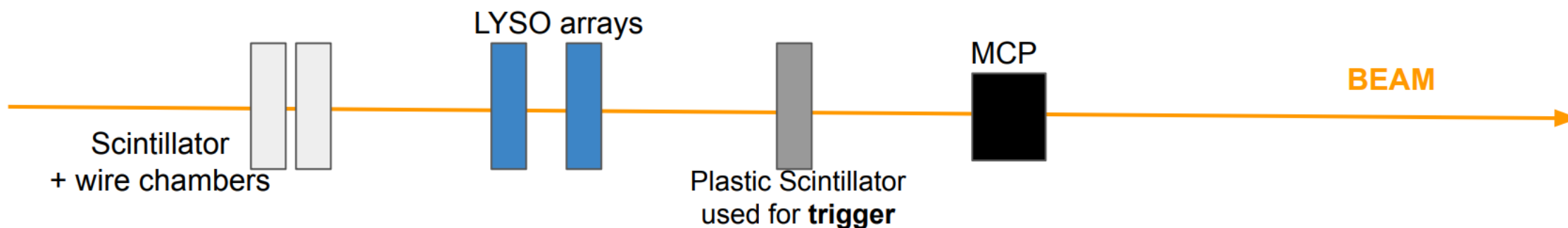
Energy linearization: setup

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- Measurement of LYSO arrays, irradiated and non-irradiated SiPMs using TOFHIR2B
- Configuration:
 - LYSO arrays + SiPMs & TECs
 - **TOFHIR2B**
- Temperature: +10°C, -33°C
- Beam: Pions wide beam (~70% pions, ~15% protons, ~5% electrons and ~10% others)
- Test irradiated SiPMs (HPK) with TECs:
 - 0, 1e14, 2e14 irradiated fluence
- HPK:
 - non-irr: LYSO528 type2 15um
 - 2e14: LYSO796 type2 15um
 - 1e14: LYSO802 type2 15um
- FBK:
 - 1e14: LYSO803 type2 15um
 - 2e14: LYSO797 type2 15um



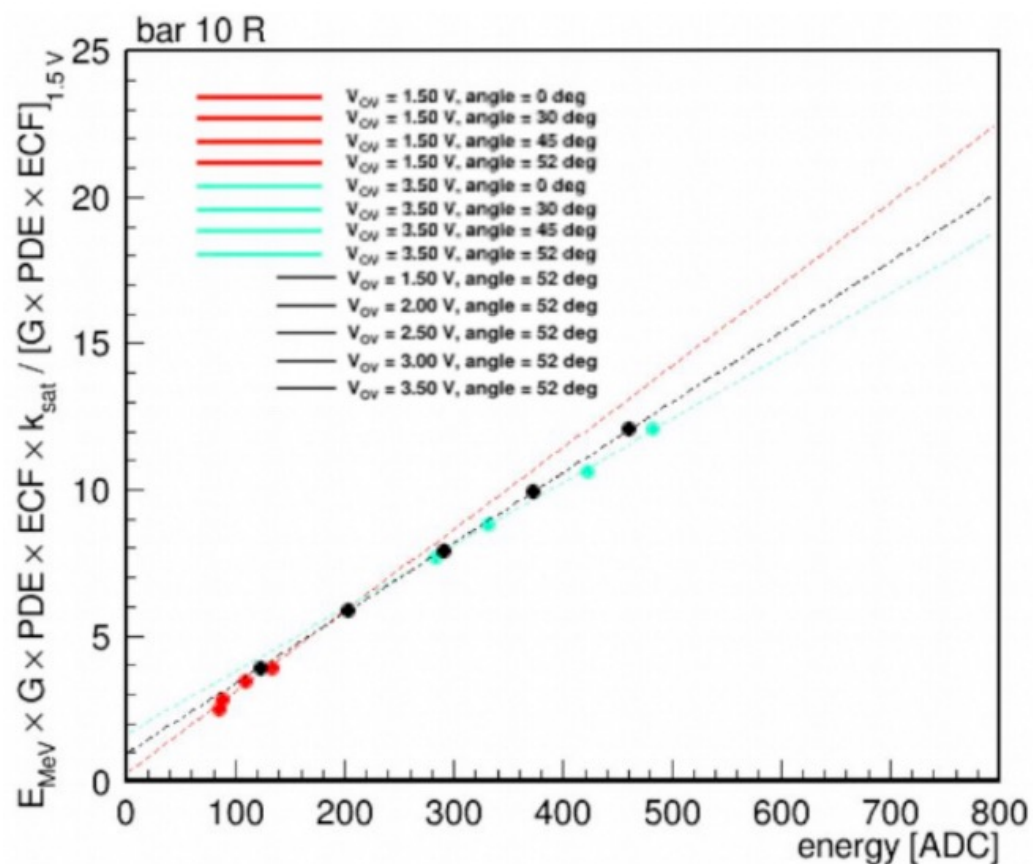
- Set up in **CERN**

Energy linearization: results



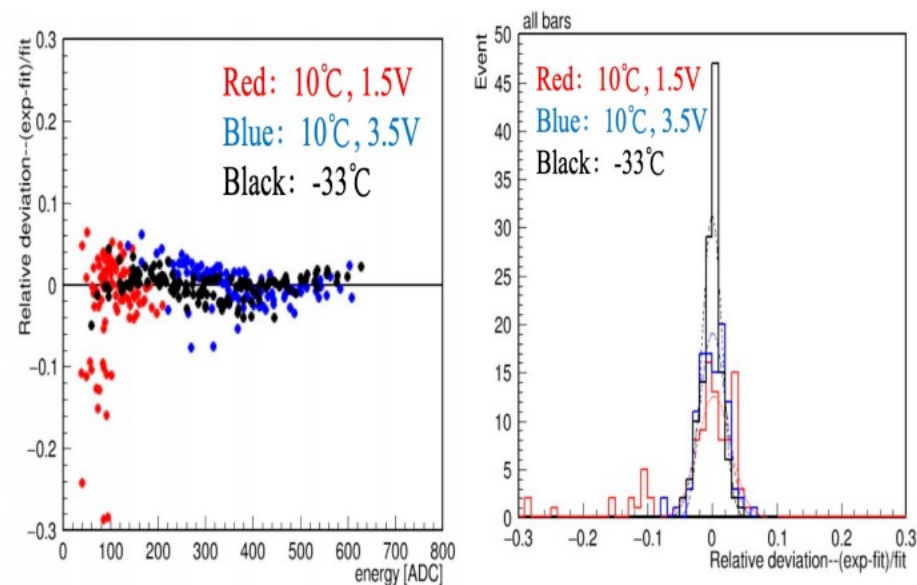
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- At the same temperature, the linearity is relatively high, and **energy spread** is about 1.5%~2.5%



$f(x) = ae^{-\frac{(x-b)^2}{2c^2}}$	b	c
10°C, 1.5V	0.0026	0.0257
10°C, 3.5V	0.0004	0.0205
-33°C	-0.0004	0.0149

The fraction of red point in (-0.1, 0.1) is 91/104



Energy linearization: summary



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Performed test beam analysis to study the **energy response** of MTD BTL sensor modules with the data taken from June22nd

- Found good linearization of the energy digitized by TOFHIR2B ASIC
- Observed radiation effects roughly consistent with expectations

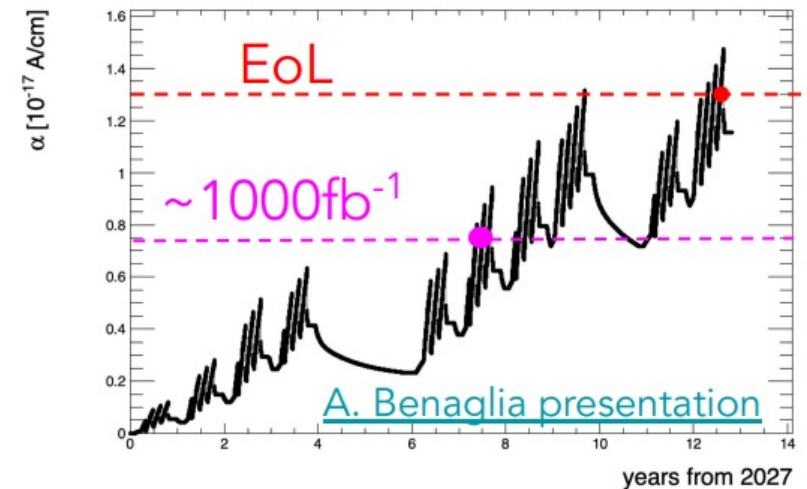
Temperatures: Calculating

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- Annealing factor evolution for **irradiated** SiPMs during HL-LHC (-45°C)
 - The expected value of damage rate parameter α is 1.3E-17 A/cm
- PDE(photon detection efficiency), Gain losses and DCR(dark count rate) vs V_{ov} caused by irradiation are not considered:
 - $I_{\text{dark}}/I_0 \sim (1.9)^{dT/10}$
 - ✓ $2E14 \rightarrow T(\text{EoL}) = 10\log 1.9(1.3/0.68) + (-45)^\circ\text{C} = -35^\circ\text{C}$
 - ✓ $1E14 \rightarrow T(\text{EoL}) = 10\log 1.9(1.3/0.34) + (-45)^\circ\text{C} = -24.2^\circ\text{C}$
 - ✓ $1E13 \rightarrow T(\text{EoL}) = 10\log 1.9(1.3/0.034) + (-45)^\circ\text{C} = +11.7^\circ\text{C}$
 - ✓ $2E14 \rightarrow T(\text{mid-life}) = 10\log 1.9(0.8/0.68) + (-45)^\circ\text{C} = -42^\circ\text{C}$
 - ✓ $1E14 \rightarrow T(\text{mid-life}) = 10\log 1.9(0.8/0.34) + (-45)^\circ\text{C} = -32^\circ\text{C}$
 - ✓ $1E13 \rightarrow T(\text{mid-life}) = 10\log 1.9(0.8/0.034) + (-45)^\circ\text{C} = +4^\circ\text{C}$



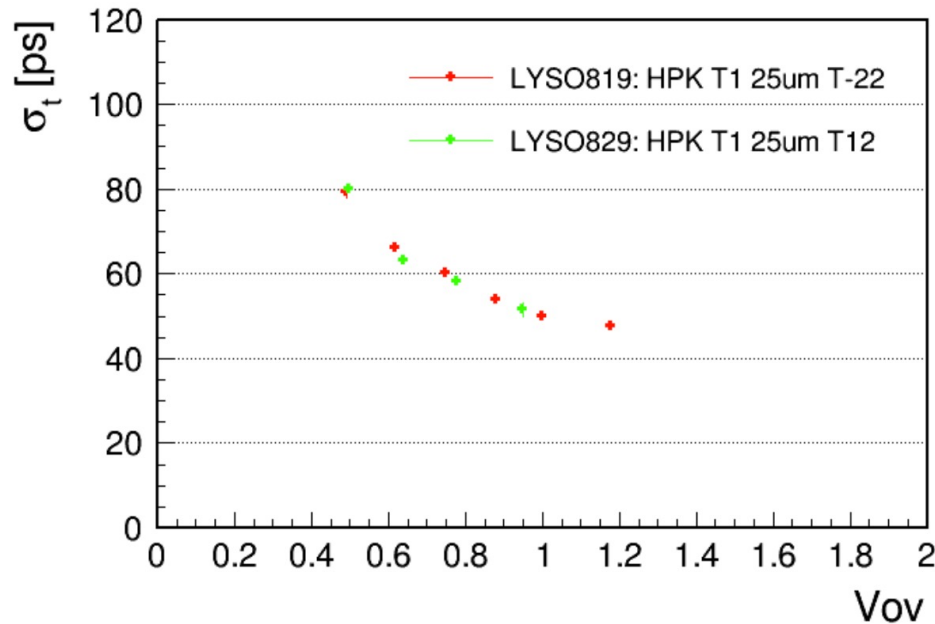
Temperatures: time resolution



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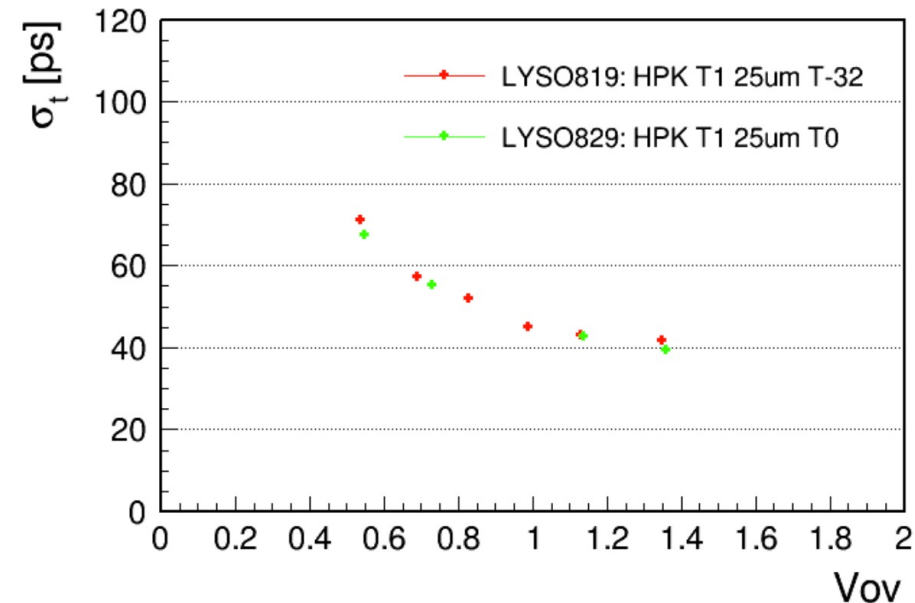
➤ Comparison of time resolution(1E14 vs. 1E13)

- in EoL condition



- The time resolution for both configuration both go better when Vov increasing;
- The performance of two configuration meet very well.
- Time resolution ~ 50 ps

- in mid-life condition



- The time resolution for both configuration both go better when Vov increasing;
- The performance of two configuration meet very well;
- Time resolution ~ 40 ps.

Temperatures: Summary

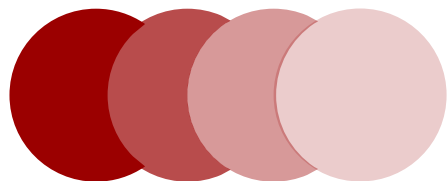


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- With the assumption of $\alpha(\text{EoL}) = 1.3\text{E-}17 \text{ A/cm}$ and $\alpha(\text{mid-life}) = 0.8\text{E-}17 \text{ A/cm}$, the temperatures to emulate the two conditions under $1\text{E}14$ and $1\text{E}13$ fluence are calculated;
- The time resolutions of the two set of configuration are very close to each other. Both the two configurations can be used to emulate EoL condition and mid-life condition.
- The time resolution for EoL emulation can reach about 50 ps. The time resolution for mid-life condition emulation can reach about 40 ps.



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03 Coupling and QA/QC

Gluing Work and QA/QC Test

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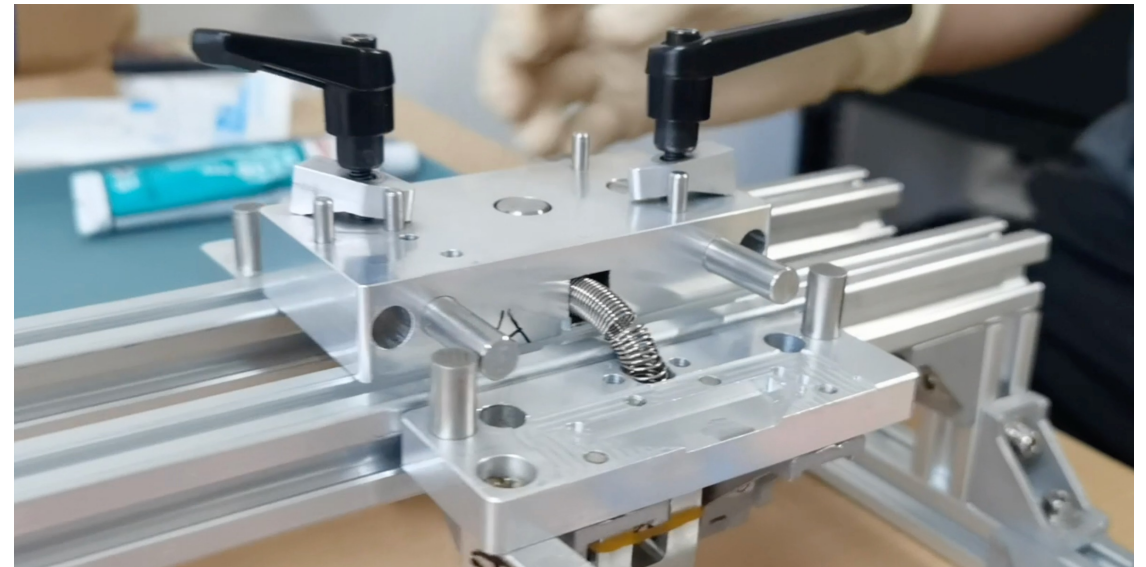
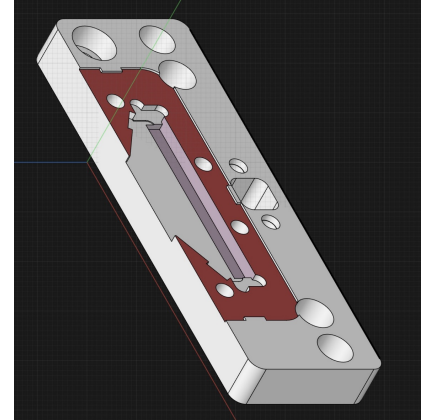
Based on the original LYSO+SiPM gluing tool designed by UVA

modified the SiPM **cups**:

- Magnets used to fix mask
- The shape and depth can hold a mask
- The groove matches the TECs

A simple **shelf** is made to hold the gluing tool

- Open the SiPM cups and place them on the shelf for the preparation of glue and the gluing process
- Given the springs, the two cups cannot stay horizontally. Thus, a rubber band is introduced to balance the spring

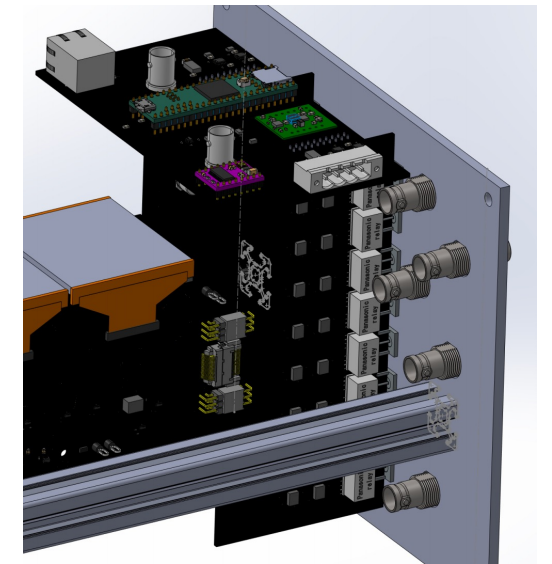
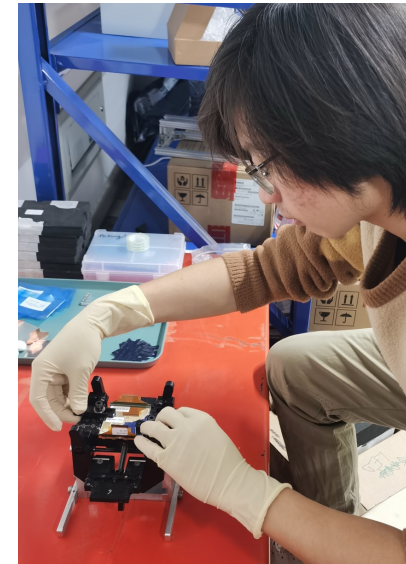
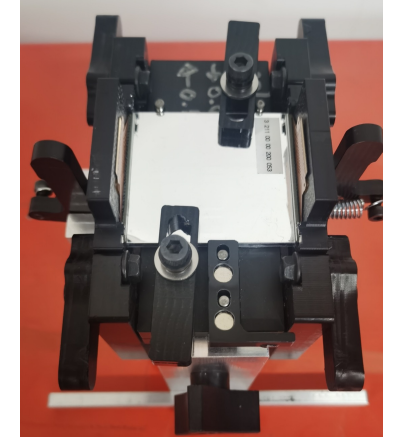


Gluing Work and QA/QC Test



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- Some advantages of the coupling workplates
 - Simplify the coupling steps (the preparation of glue and the gluing process)
 - Effectively reducing the time the adhesive is exposed to the air after gluing; reducing the probability of SiPM falling off the workpiece
 - Improve **reliability** in multiple ways
- Using a new gluing tool with similar design for gluing small batch modules for test
- Further tests will be conducted afterwards
 - **QA/QC test** is an important method for checking the gluing effect



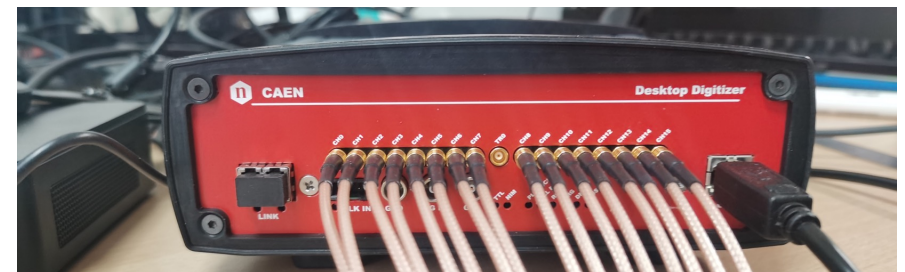
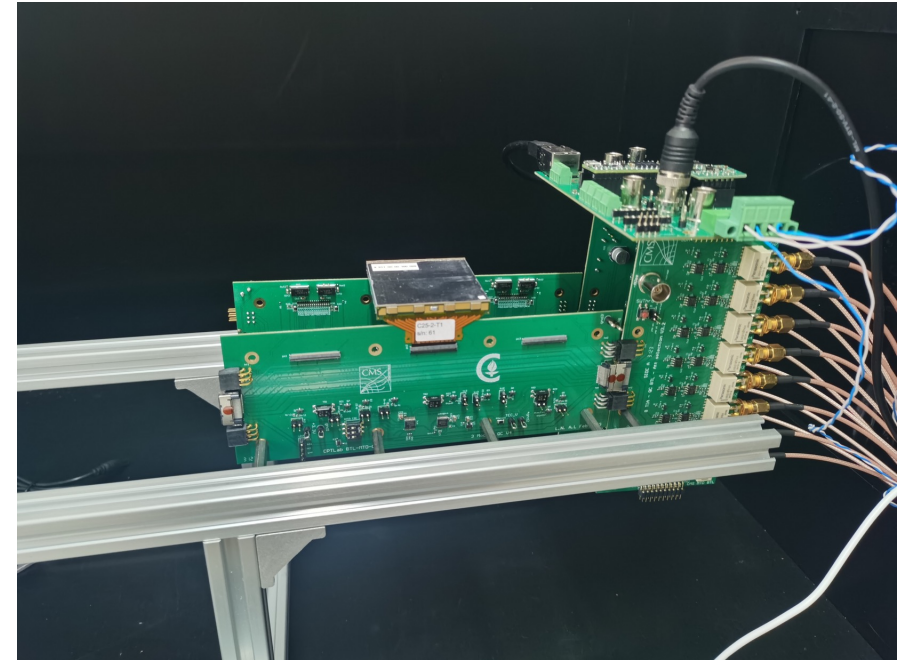
Gluing Work and QA/QC Test



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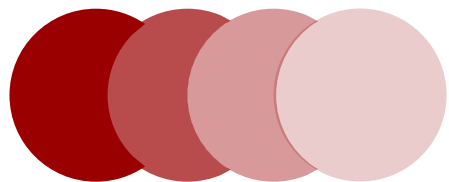
The BTL QA/QC jig :

- Designed to test up to 12 LYSO arrays at a time for quality assurance during gluing procedure.
- Hardware organization and theory of operation:
 - **3 Module Boards:** connecting to the actual modules and controlling the HV relay
 - **Amplifier boards:** taking 8 analog signals from the SiPMs and amplifying them to be able to read out by the CAEN digitizer
 - **Control Board (with teensy 4.1):** talking to the other boards to control the HV relays, attenuation relays, as well as to read out the RTD and thermistor temperatures, etc
 - **DT5742 CAEN digitizer:** Obtaining 16 channels at a time
 - **Dark Box, support and cooling system:** Providing a constant temperature dark environment and easy control of experiments





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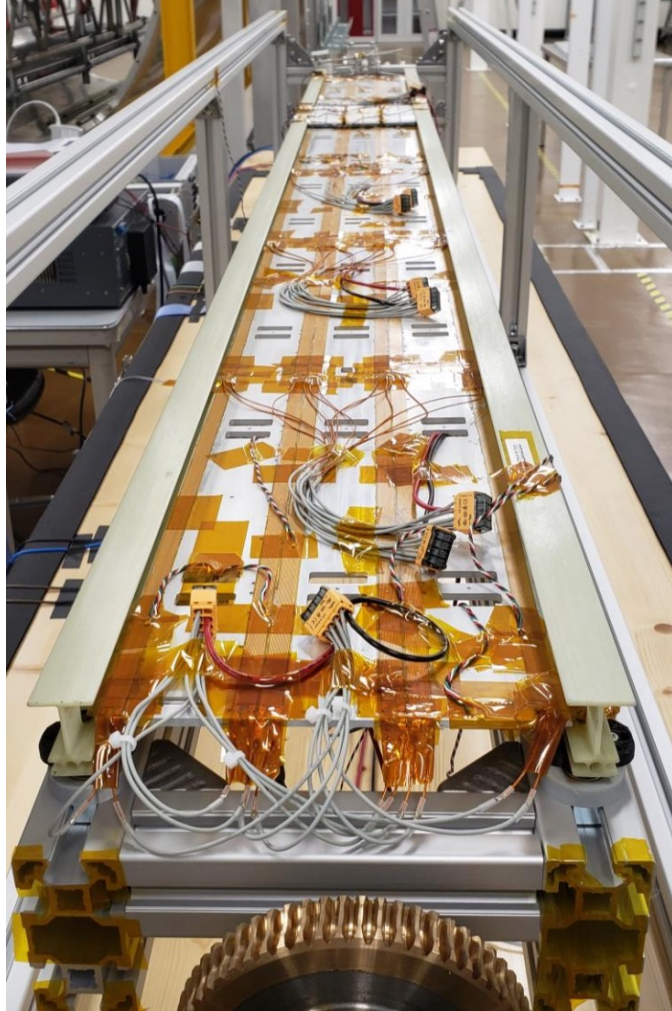
04 Cooling Plates and Thermal Test

Cooling plates and Spitroast

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(PKU)



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Structure

- $2.5 \times 0.2 \times 0.03\text{m}$ Aluminum plate with 2 embedded cooling loops.
 - Plate segmented in 6 pieces (RUs).
- Thermal paste between cooling plate and cooling loops.
- Cooling loops are held in place with laminas that are attached with screws to the cold plate.
- At Peking University, we have produced a batch of cooling plates(5 sets) for test
- The rotating bracket "spitroast" has also been put into use,
 - making it more convenient to carry out on the front and back sides of the plates and assist in transportation



Cooling plates: Thermal test

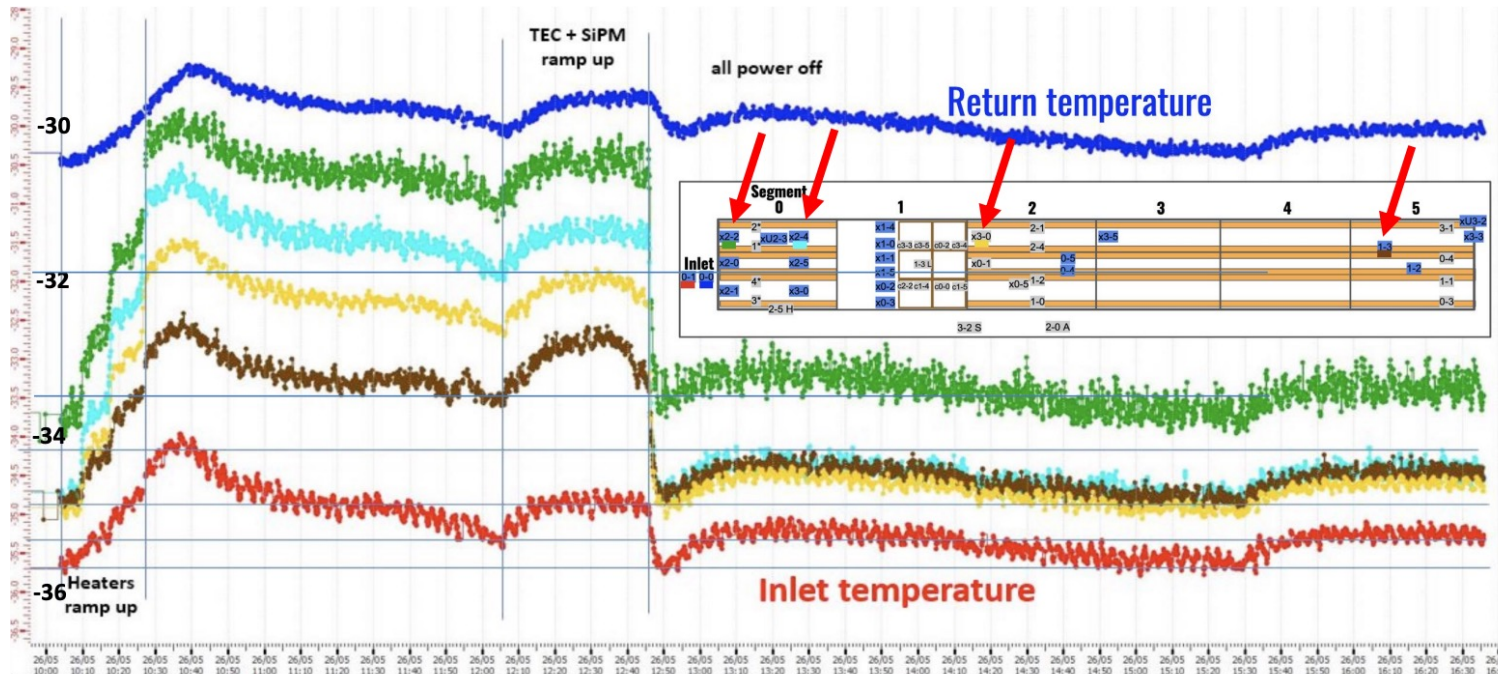
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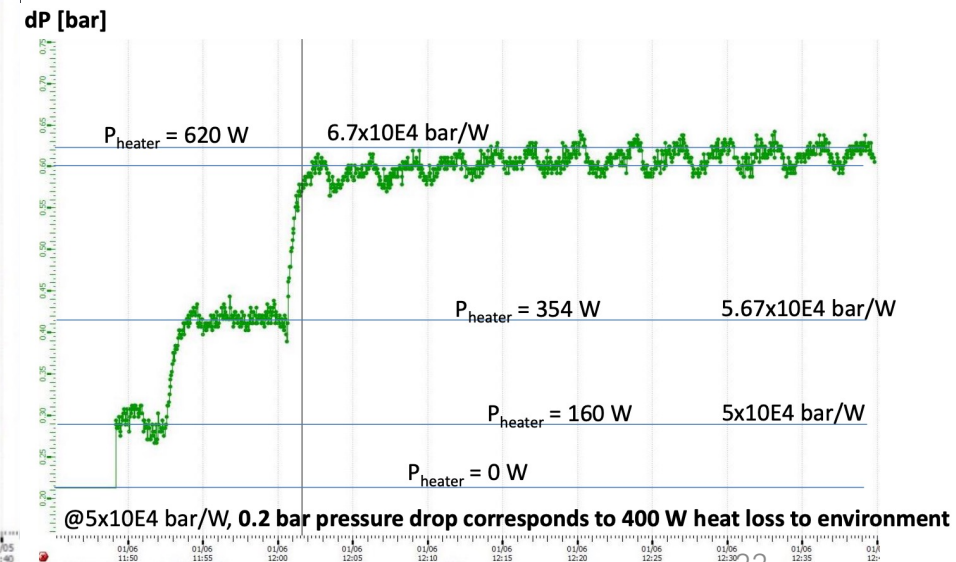
Tray cold test

- dP capillary ~ 21.2 bar, $T \sim -34$ °C, CO_2 flow ~ 6 g/s.
- Measurement on the tray:
 - Inlet ~ -36 °C; Outlet ~ -30 °C; dT along the tray ~ 2 °C (somewhat larger than expected 1 °C)
- Plan
 - Add a loop for the dry air; Add insulating material to the surface of tray; Attach more temperature sensors to the inlet/outlet.



Environment loss:

dP in BTL loops vs Heater Power



Cooling plates: Thermal test



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CO₂ cooling and tray thermal management **meet expectation.**

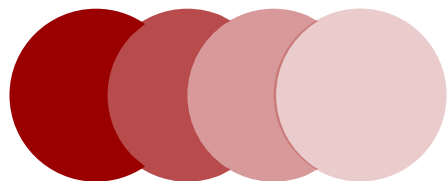
- Thermal gradient along the tray larger than expected.
- Plan: Add a loop for the dry air; Add insulating material to the surface of tray; Attach more temperature sensors to the inlet/outlet.

Environmental losses are important in our test setup – more refinements needed making it more similar to final layout in CMS.

- At 5×10^{-4} bar/W, 0.2 bar pressure drop corresponds to 400 W heat loss to environment.



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05 Summary

Summary



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Summary

- Optimized sensor design through test beam(Energy linearization, LYSO, SiPM, Temperature), finalize plan, and pass CMS review
- Improved the coupling work of LYSO SiPM, simplify the scheme and improve system reliability
- Completed the construction of the sensor module QA/QC and conduct small-scale module tests
- The thermal test of the cooling system show that the cooling plates and TEC design scheme meet the requirements

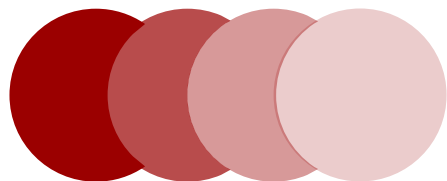
Plan

- Continue with TB analysis for comparion of different SiPM vendors
- Improve the design of LYSO+SiPM coupling work
- Further tests of the cooling plates system
- Start assembling the sensor module
- Improve sensor module QA/QC and conduct large-scale tests

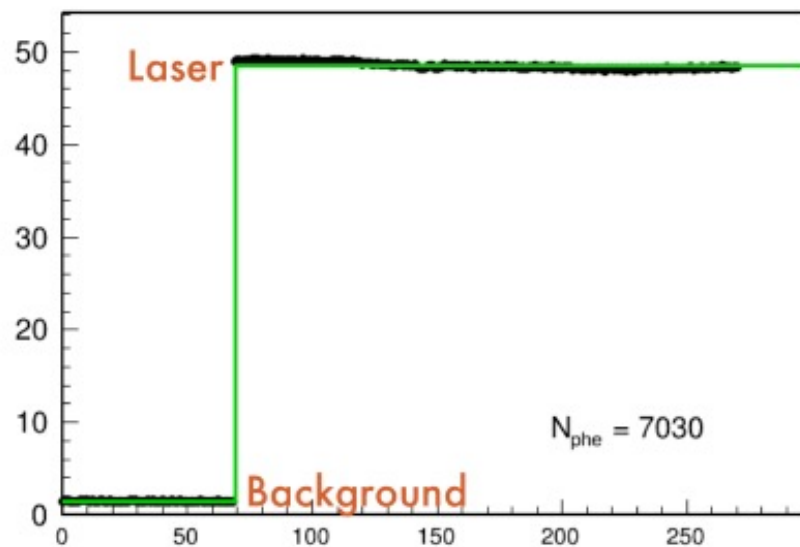
Thanks for your attention!



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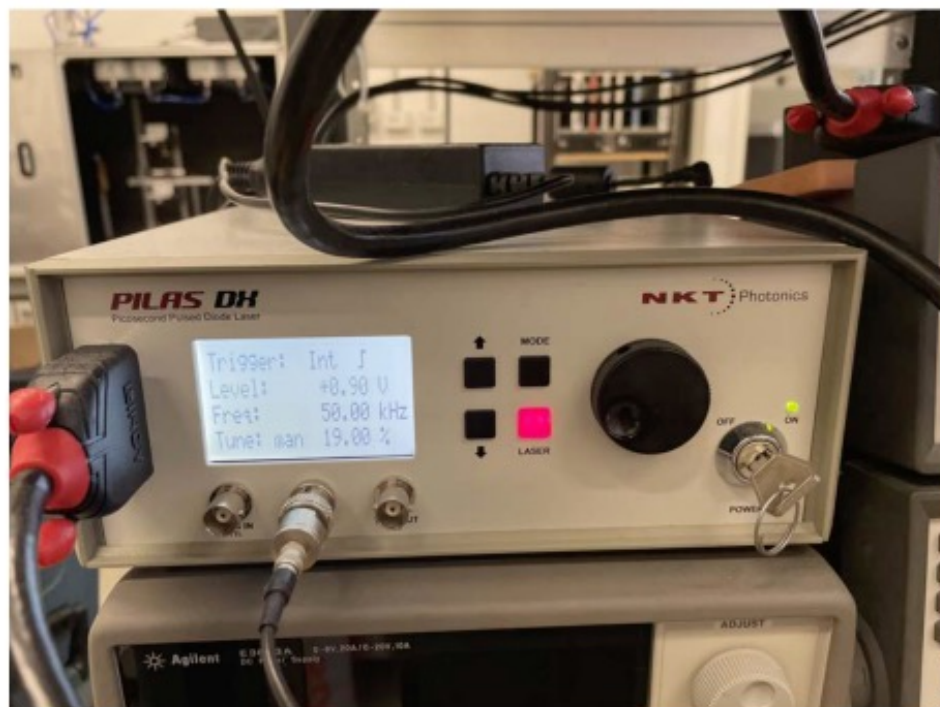
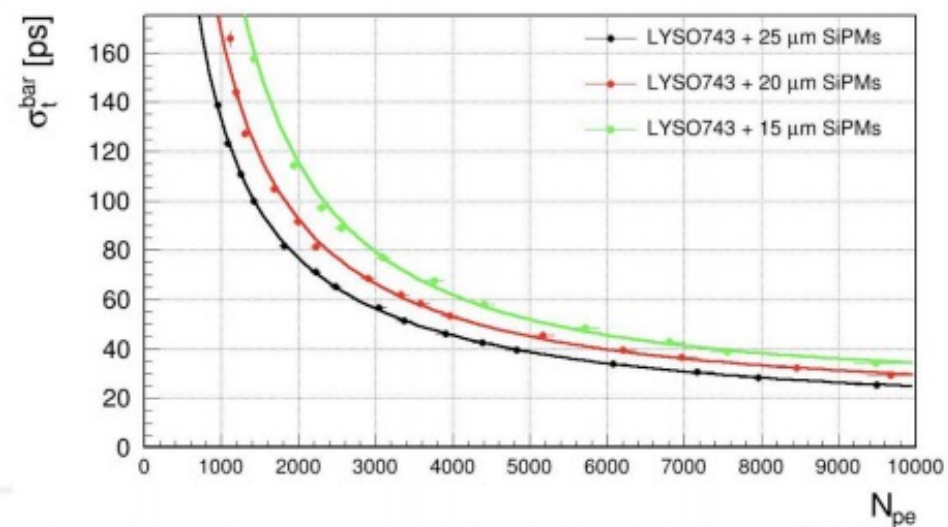
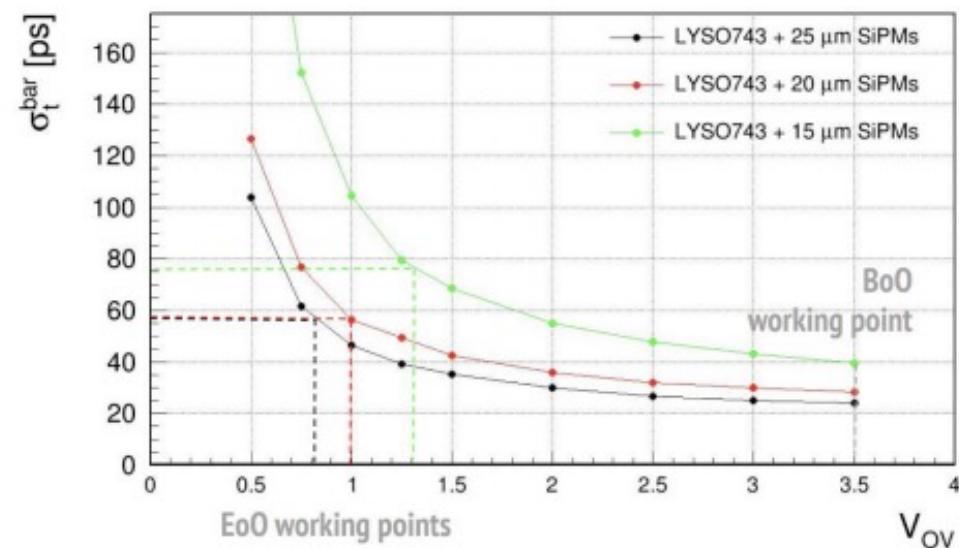


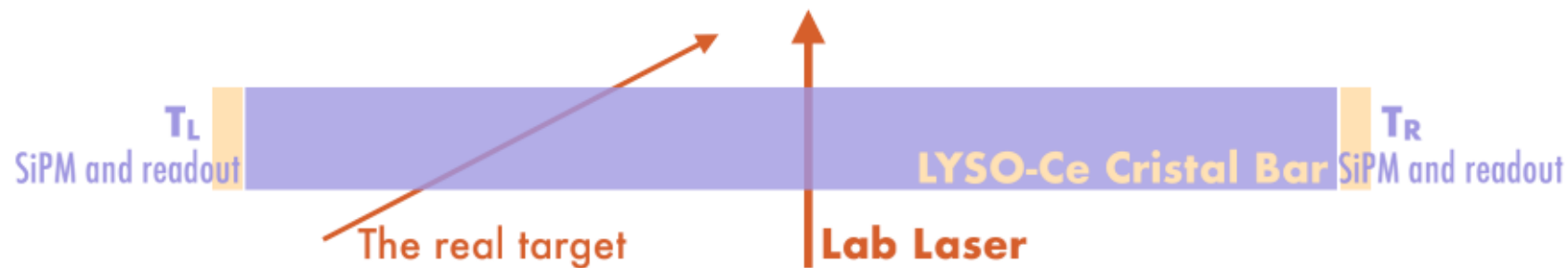
Back up



• Laser intensity tuned to reproduce the expected Npe at 3.5 V (LO-1250 pe/MeV for optimized LYSO+15 μ m SiPMs)

- $N_{pe} = 4.2 \text{ MeV} \times 1250 \text{ pe/MeV} = 5250 \text{ pe}$ for 15 μ m
- $N_{pe} = 4.2 \text{ MeV} \times 1250 \text{ pe/MeV} \times \text{PDE}_{20\mu\text{m}} / \text{PDE}_{15\mu\text{m}} = 7950 \text{ pe}$ for 20 μ m
- $N_{pe} = 4.2 \text{ MeV} \times 1250 \text{ pe/MeV} \times \text{PDE}_{25\mu\text{m}} / \text{PDE}_{15\mu\text{m}} = 8900 \text{ pe}$ for 25 μ m

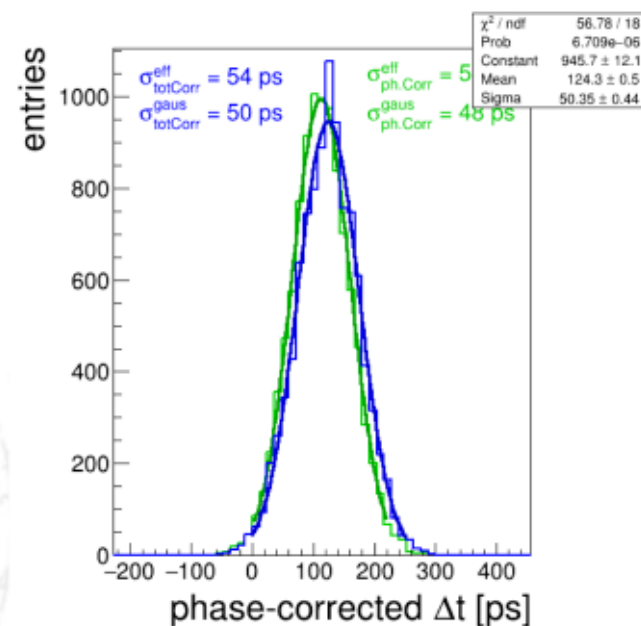


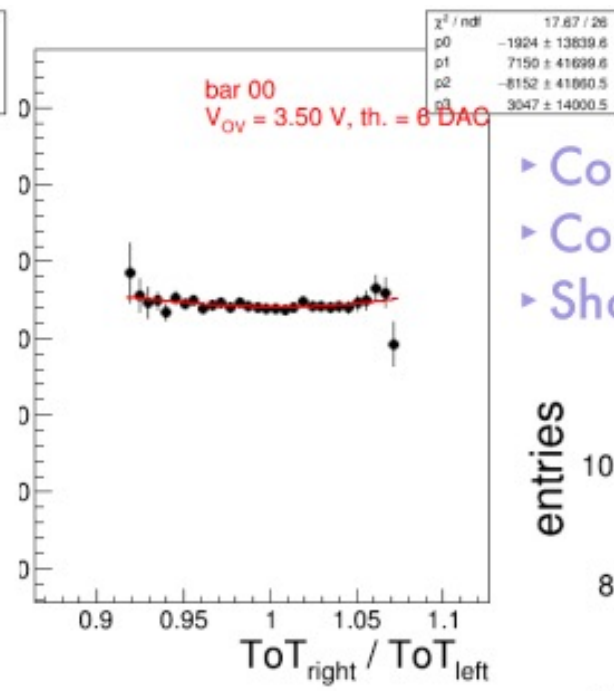
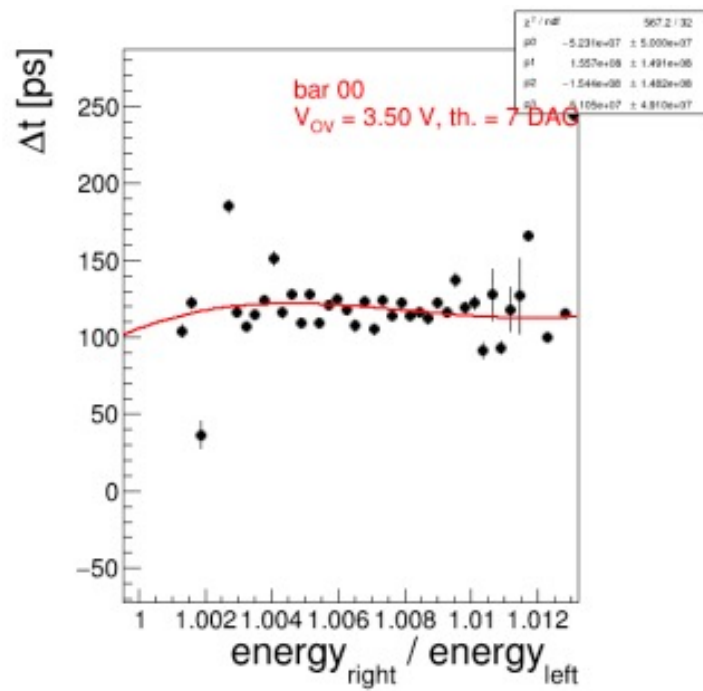


$$T_{ave} = 1/2(T_L + T_R) \quad \sigma_{ave} = 1/2\sqrt{\sigma_L^2 + \sigma_R^2}$$

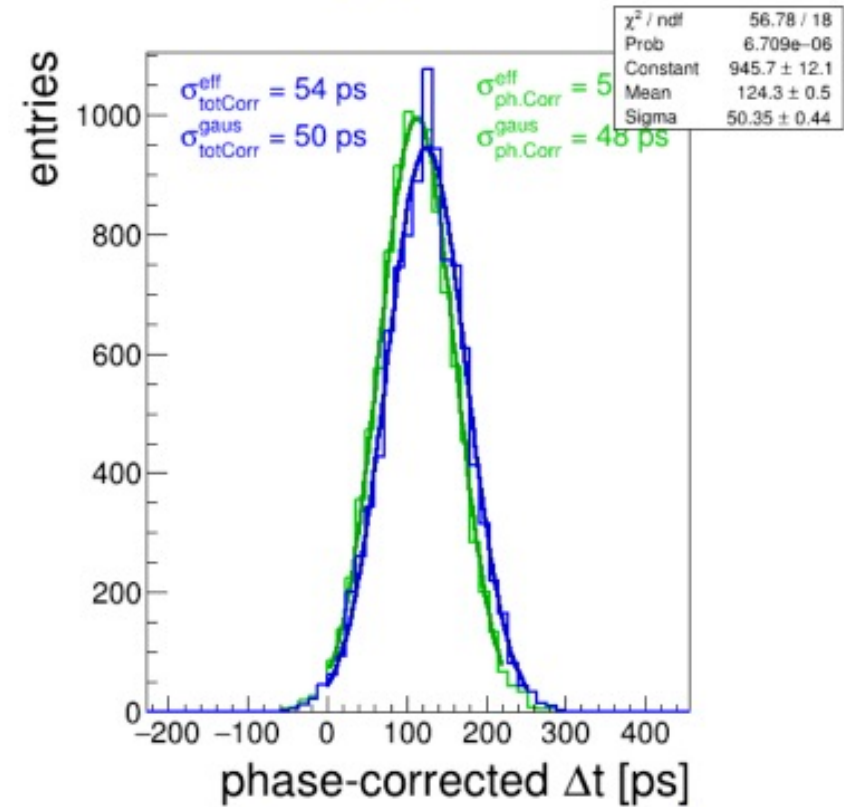
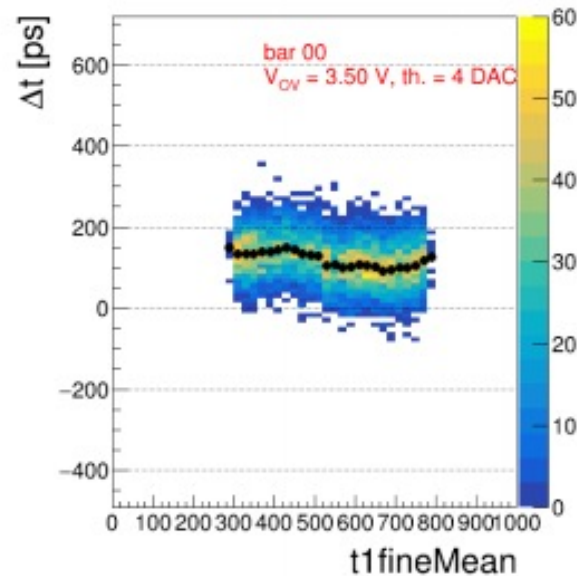
$$\sigma_{diff} = 2 \times \sigma_{ave}$$

$$T_{diff} = T_L - T_R \quad \sigma_{diff} = \sqrt{\sigma_L^2 + \sigma_R^2}$$





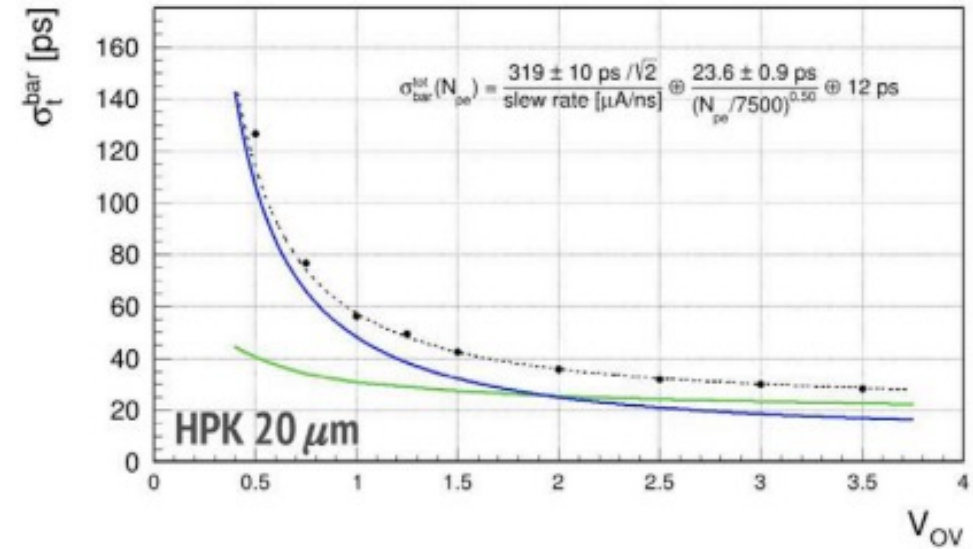
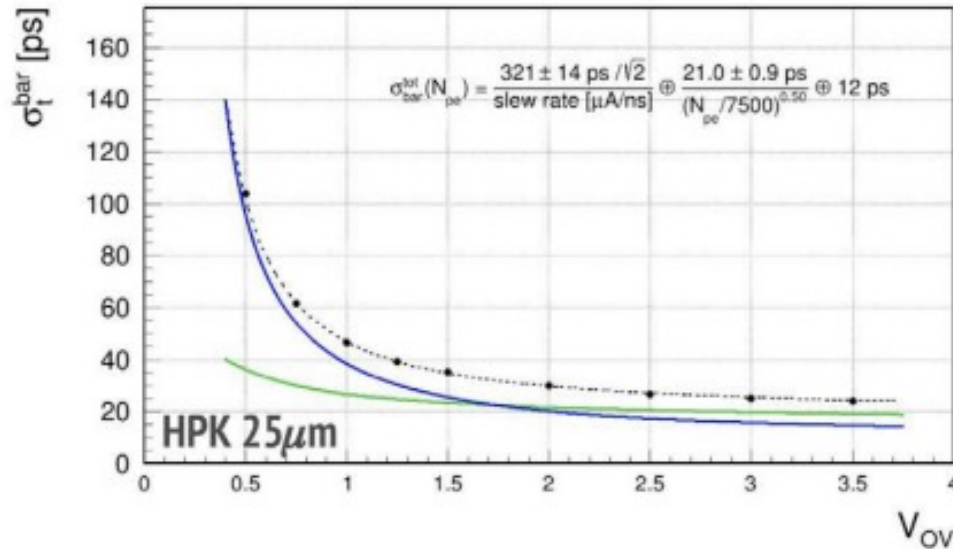
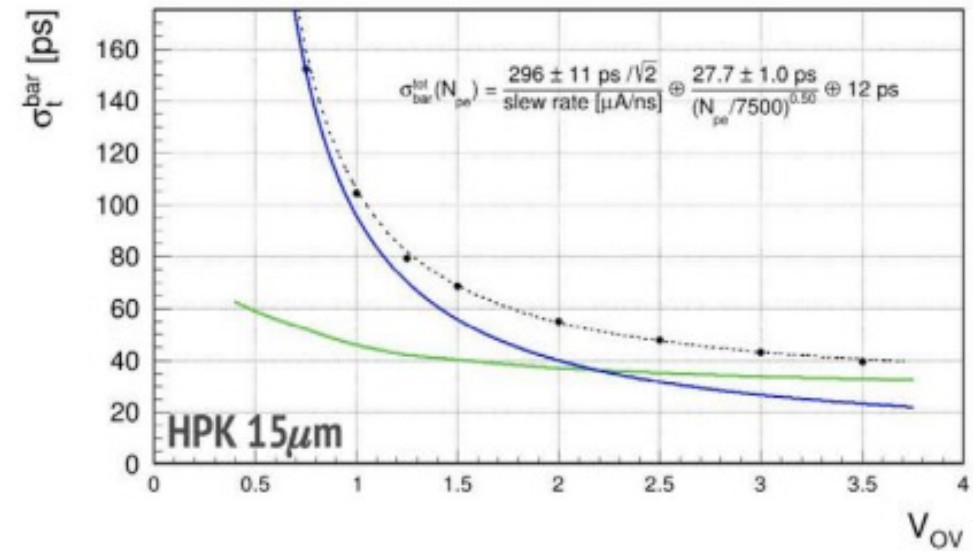
- Correction over energy difference
- Correction over ToT
- Should be highly correlated



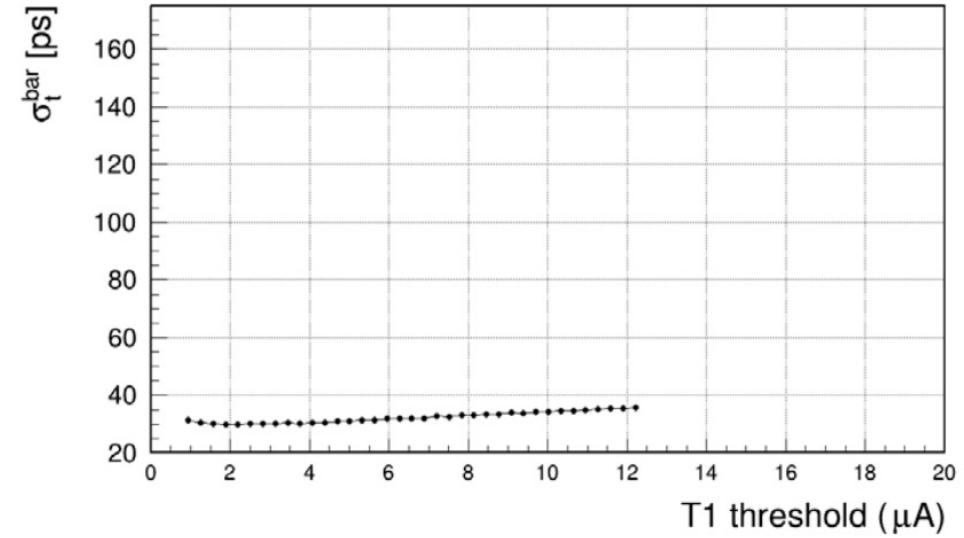
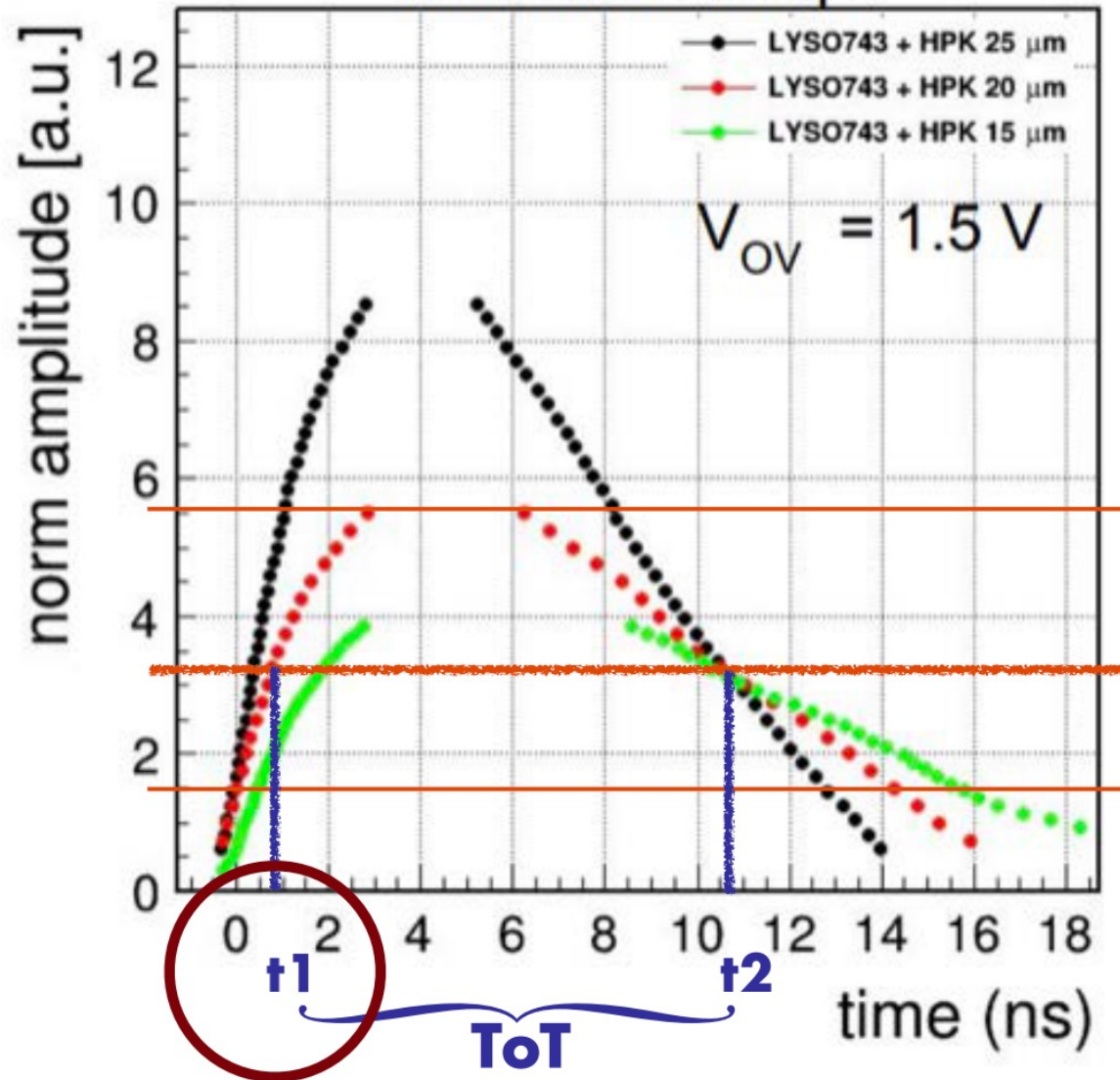
- Correction of the starting point in the triggering window
- Secrets in electronics

Splitting noise and stochastic contributions

- Fit total time resolution vs V_{OV} with sum in quadrature of stochastic and noise terms
- Stochastic term ~ 28 ps for 15 μm , compatible with previous estimations
- Stochastic term for 20, 25 μm smaller (thresholds effect?)
- Noise term smaller than measured in the past (420 nA)
- however, we are using a different board (T2TB v2)

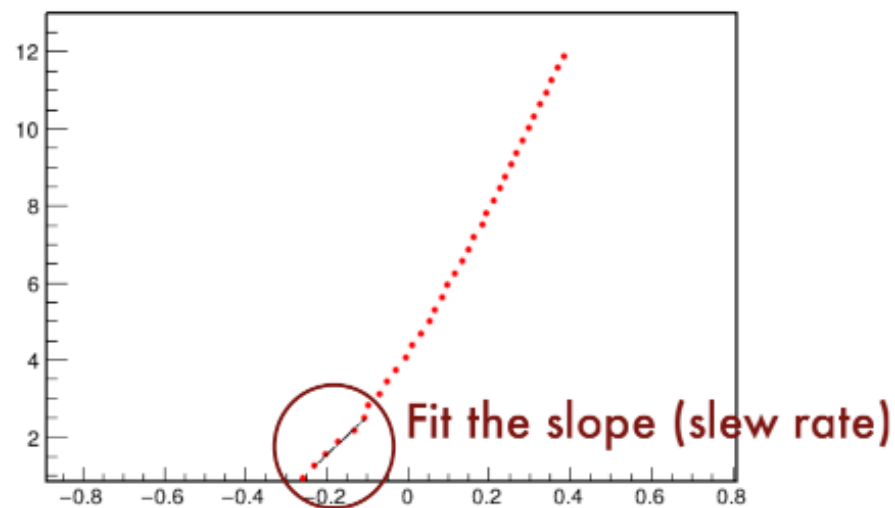


Average pulse shapes normalized to Npe



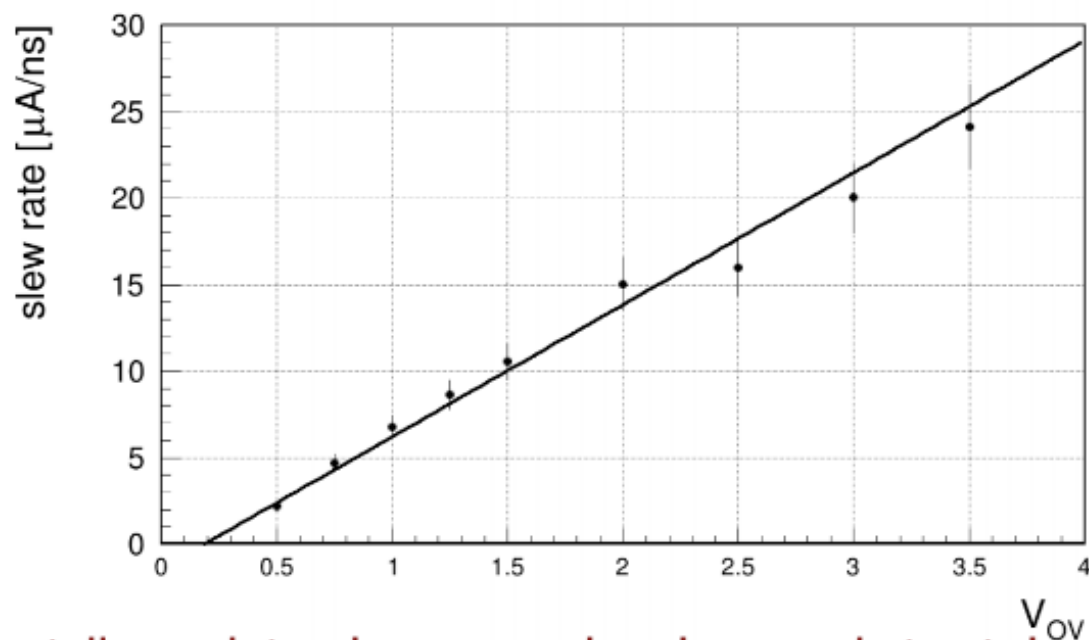
Thresholds

- Find the threshold that can minimize the t-resolution
- Understand how performances are effected



$$\sigma_t^{pe} = \frac{A}{\sqrt{N_{pe}}}$$

At the beginning of the pulse shapes (near the optimized threshold)



$$\sigma_t^{noise} = \frac{\sigma_N}{dA/dt}$$

Partially explains the reason that the t-resolution is better at higher V_{ov}

LYSO selection



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- Plot the “expected energy” vs. the measured MIP Landau MPV in ADC, as measured by the TOFHIR2B

- energy [ADC] (x-axis):
MIP peak obtained by Landau fitting

- “expected energy” (y-axis):

$$E_{\text{dep}} [\text{MeV}] \times G \times \text{PDE} \times \text{ECF} \\ \times k_{\text{saturation}} / \text{Norm}$$

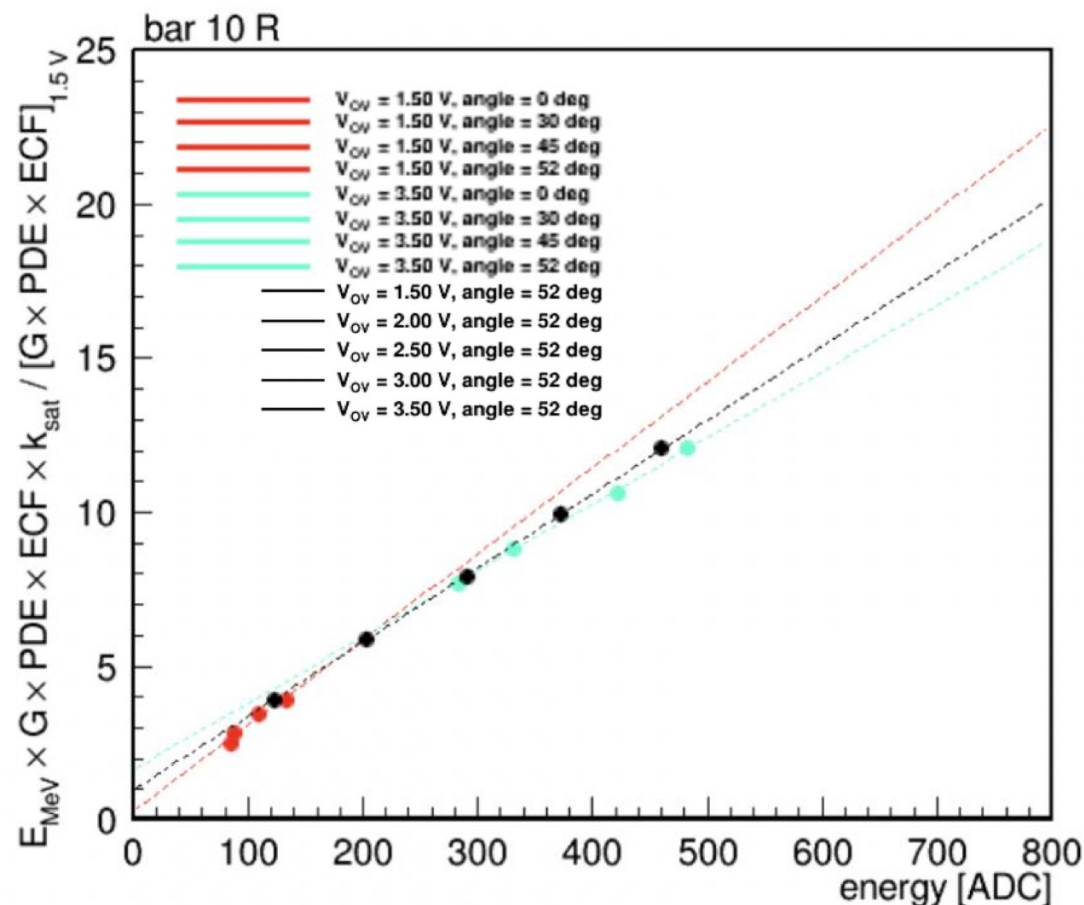
$$E_{\text{dep}} = 0.86 \text{ MeV/mm} * 3 \text{ mm} / \cos(\text{angle})$$

G = sipm Gain

PDE = photon detection efficiency

ECF = excess charge factor

$$k_{\text{saturation}} = N_{\text{pixels}} \times [1 - \exp(-N_{\text{pe}} / N_{\text{pixels}})] / N_{\text{pe}} \text{ (with } N_{\text{pixels}} = 40000)$$



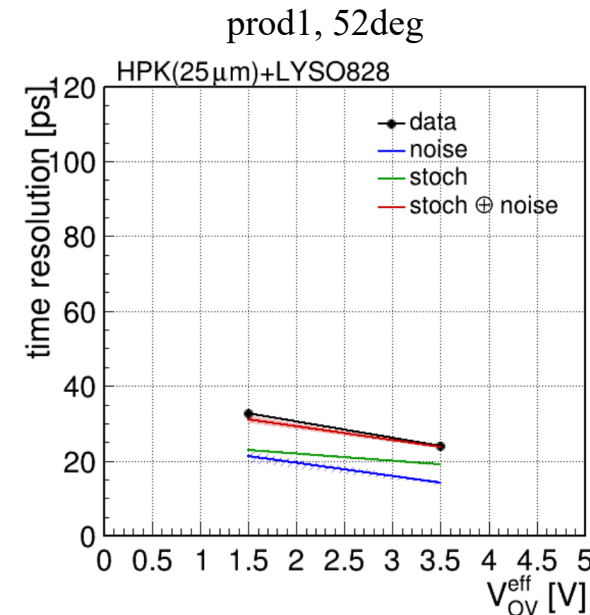
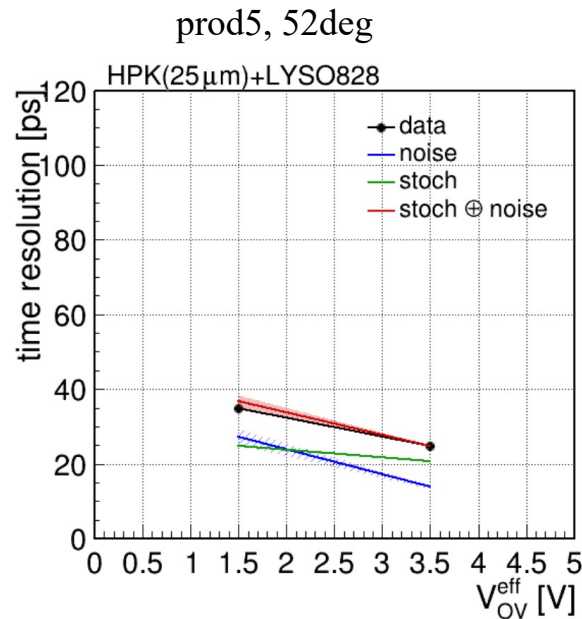
LYSO selection



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Breakdown of uncertainties

- Experience formula is used to decompose the time resolution into noise \oplus stochastic.



- So far, there is no experimental formula of Npe, so $V_{ov} = 3.50V$ is used as a reference, and the formula of PDE is used to estimate the stoch part.
- **With the increase of V_{ov} , the noise contribution decreases faster.** This is because SR is more sensitive to V_{ov} than PDE.

Damage rate parameter



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Annealing of α at fixed temperature

Damage rate parameter α for silicon devices
describes change of leakage current with fluence

[\(Alexander Ledovskoy's talk\)](#)

$$\Delta I = \alpha \cdot \Phi_{\text{eq}} \cdot M$$

Measurements described in M. Moll,
“Radiation damage in silicon particle
detectors: Microscopic defects and
macroscopic properties”, Ph.D. thesis,
Hamburg U. (1999) [Moll99]

Plot from [Moll99] (page 100)

